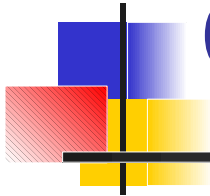




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INFLUENCE OF HYDRIDE DISTRIBUTION ON FAILURE OF ZIRCALOY-4 SHEET



Olivier Pierron, R.S. Daum, D.A.
Koss, A.T. Motta, and K.S. Chan

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Industrial Context

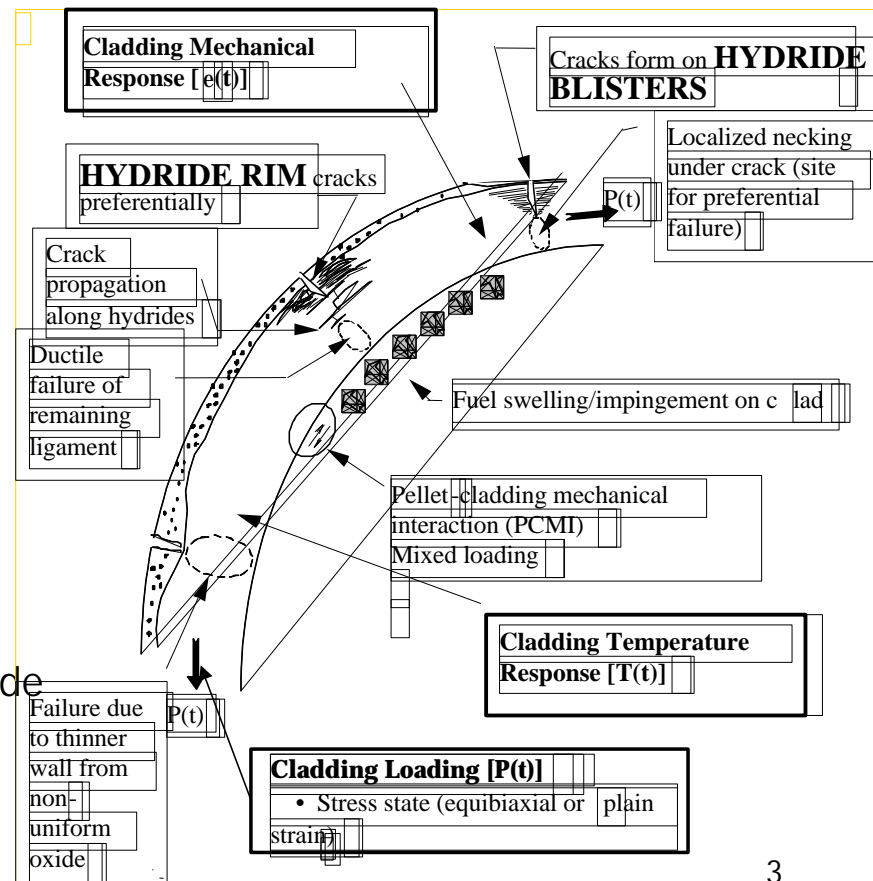
- Nuclear Industry wants to **increase fuel burnups** (residence time in reactor):
 - Fuel savings; longer fuel cycles, => higher capacity factor
 - Reduction in waste volume (less fuel assemblies for same power produced)
- Increased burnup => increased radiation damage, but also increased oxidation and associated hydriding of cladding
- **Problem:** can highly hydrided Zircaloy-4 cladding withstand severe loading conditions associated with postulated licensing accidents? (i.e., is it safe to operate fuel at high burnup, what are the limits?)



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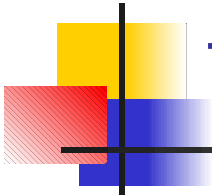
Effect of Hydrogen

- H affects cladding behavior.
- Two H distributions:
 - **Hydride "rim"**
(temperature gradient from heat flux during operation)
⇒ $\text{In}\omega\epsilon\sigma\tau\iota\gamma\alpha\tau\epsilon\delta$ (PSU)
 - **Hydride "blister"** (oxide spalling creates local "cold" spots where H aggregates)
⇒ $\text{T}\eta\iota\sigma\sigma\tau\upsilon\delta\psi$





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This Study: Hydride “Blisters”

- Experimental procedure:
 - Developed a new procedure that **simulates** the presence of hydride blisters on unirradiated Zircaloy-4 flat sheet with texture similar to tube.
 - **Plane-strain tension** (multi-axial stresses).
 - Two testing temperatures: **25°C, 300°C**.
 - Two materials: **RX, CWSR**.

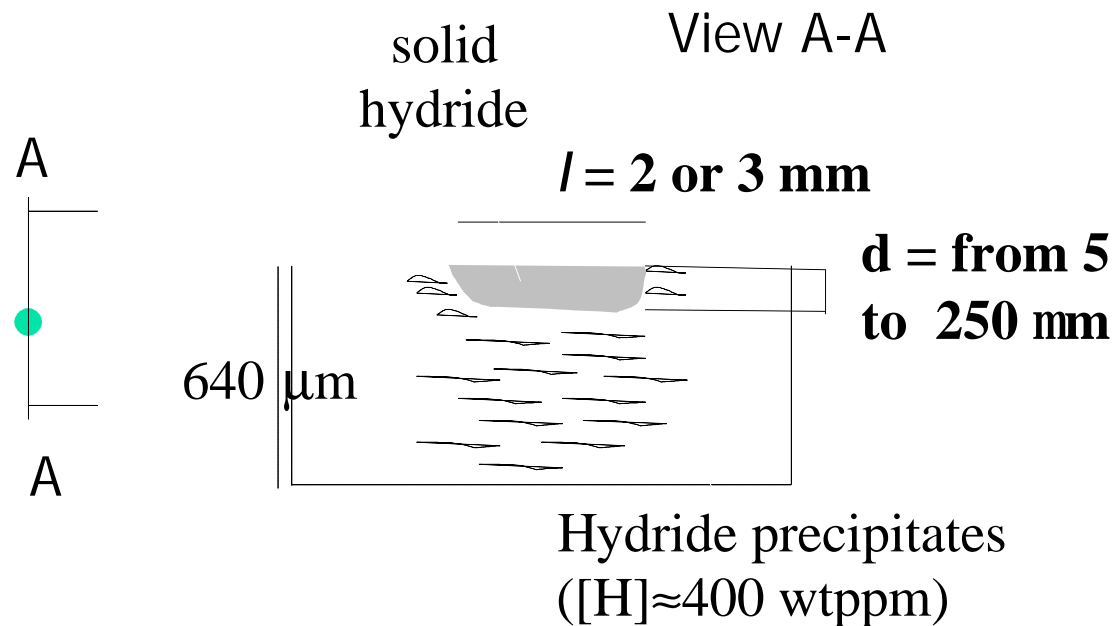


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Hydride Blister Formation

- Gas charging at 400°C

Ni coating

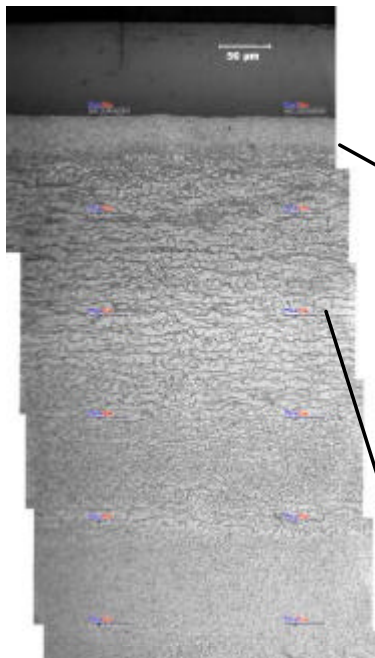




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Comparison with Cladding

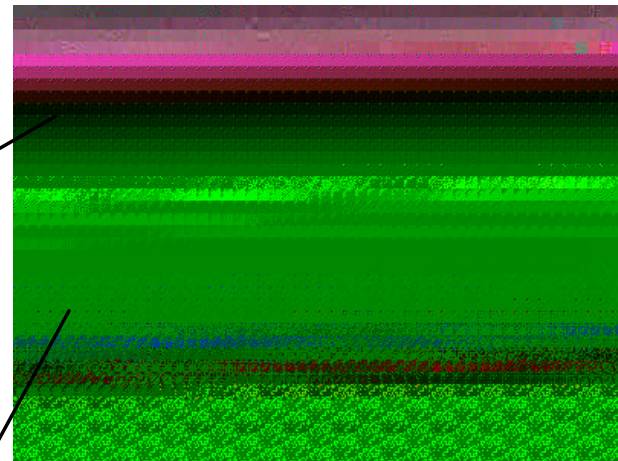
- **Irradiated cladding** (av. fuel burnup of 67 GWd/t and fast fluence of 1.3×10^{22} n/cm²)



Solid hydride

Discrete hydrides

- **PSU Hydriding** (H₂ gas charging at 400°C)



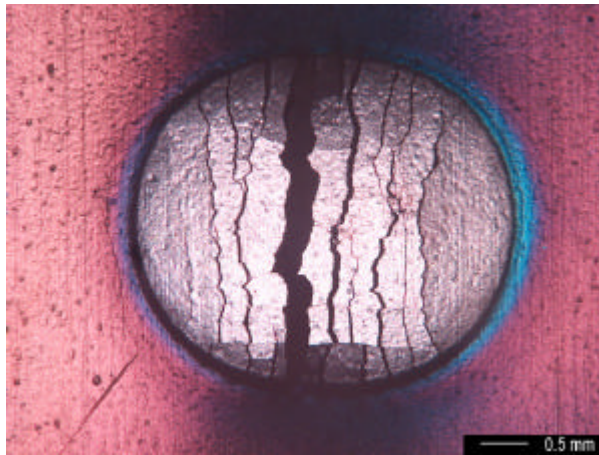
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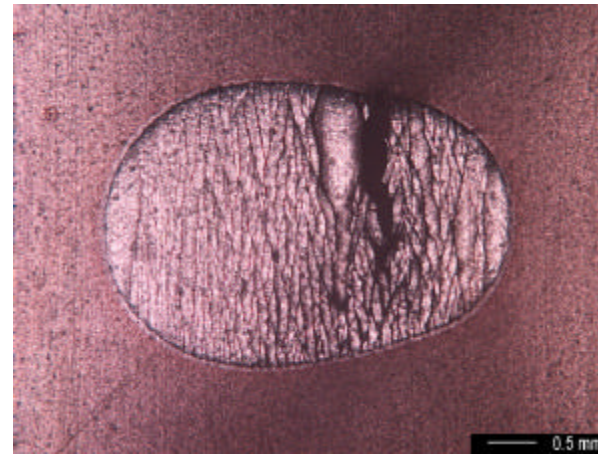
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Fracture of "Blisters"

- Formation of **micro-cracks** upon yielding (detected by Acoustic Emission).



Blister Depth: 215 μm



Blister Depth: 40 μm



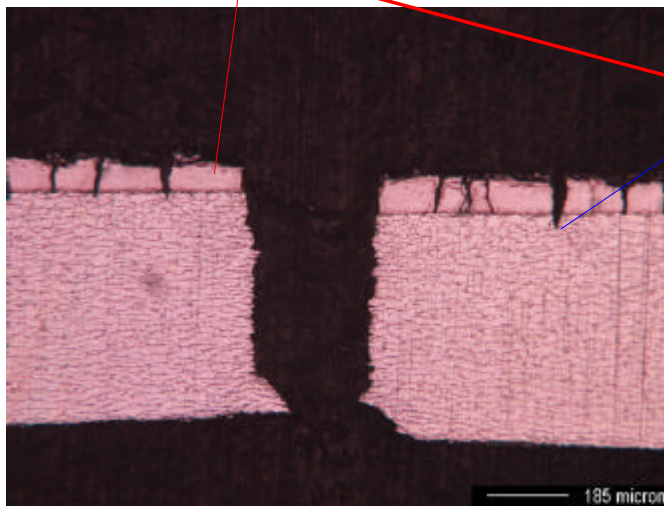
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Fracture Profiles

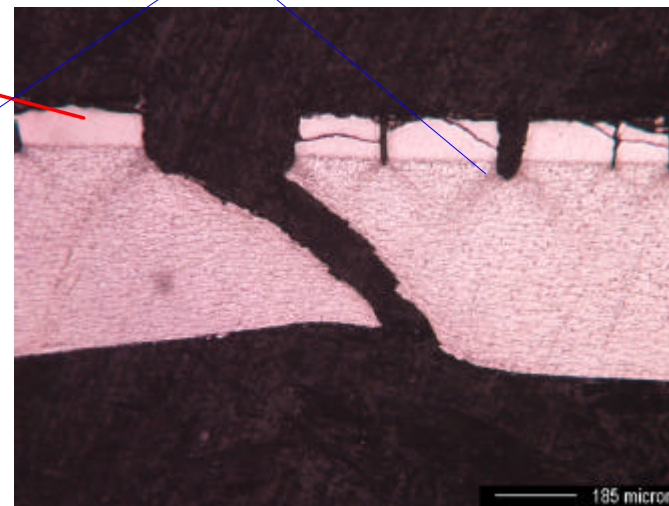
■ *Crack Growth vs. Shear Instability*

Hydride Blister

Arrested micro-cracks



25°C

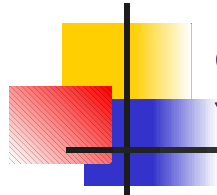


300°C

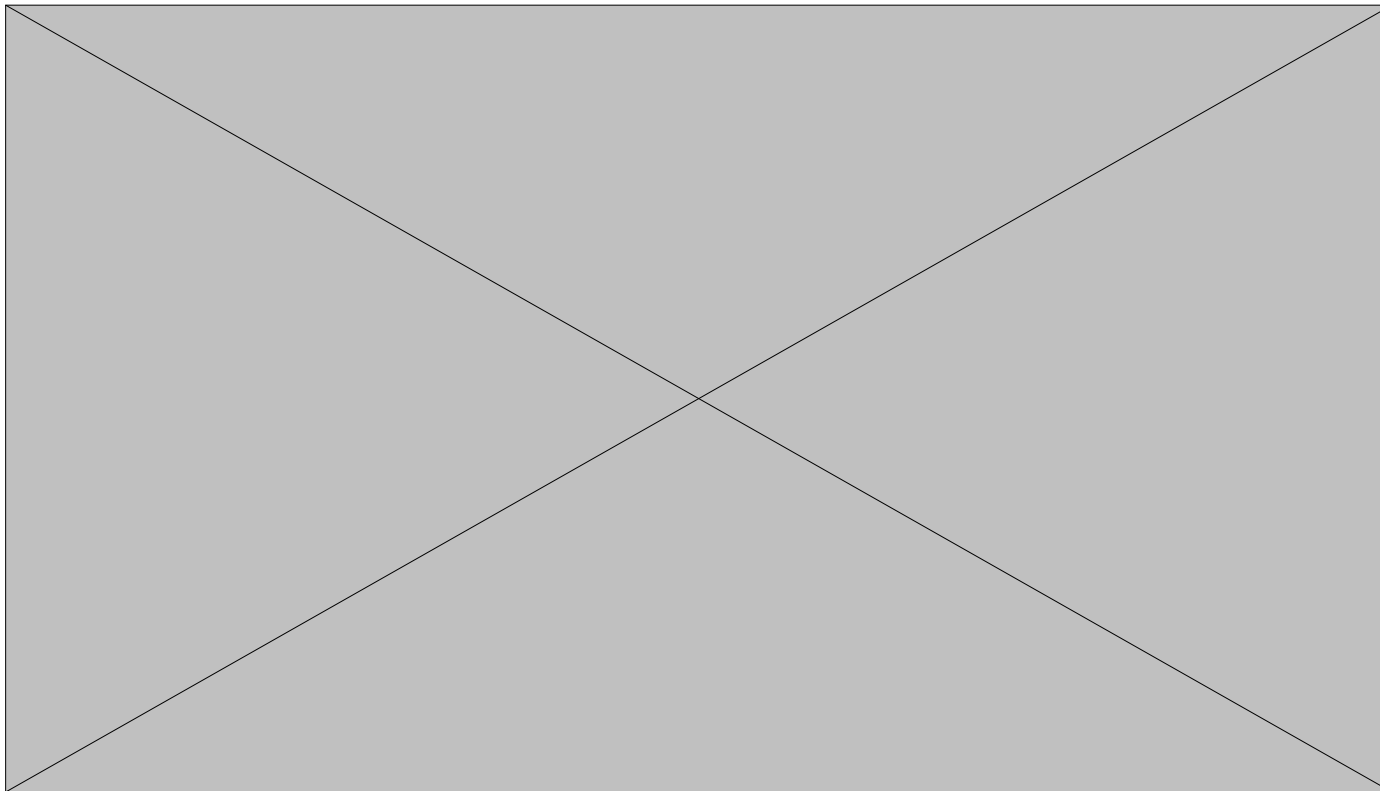
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Specimen Ductility





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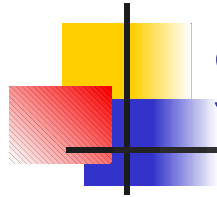


Specimen Ductility

- Significant decrease in ductility at 25°C w/ increasing blister depth > 25-50 μ m and plateau beyond \approx 120 μ m.
- Similar ductility between 2-mm and 3-mm diameter blisters.
- Hydrogen embrittlement less severe at 300°C than at 25°C for given blister depth.

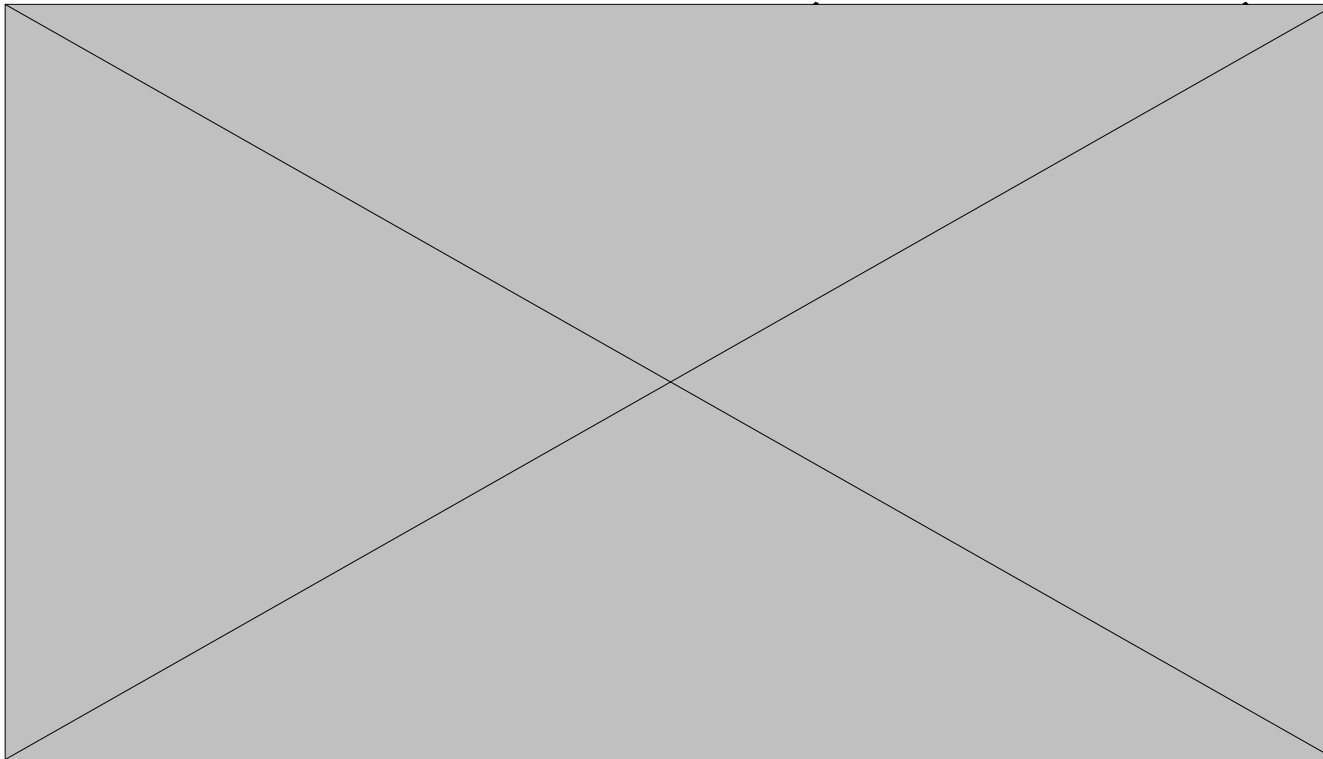


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Specimen Ductility

- Blister vs Rim for CWSR at 25°C ⇒ **Rim**





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Summary of Results

Zircaloy w/ 2 or 3 mm-diameter blisters (5 to 250 μ m thick) + hydride precipitates in substrate

- Blisters crack upon yielding.
- As blister depth \uparrow $\phi\rho\alpha\chi\tau\upsilon\rho\epsilon$ $\sigma\tau\rho\alpha\iota\nu$ \downarrow
(roughly independent of blister width)
- For given blister depth:

$$(\epsilon_{\text{frac}})_{\text{RX},25} \approx (\epsilon_{\text{frac}})_{\text{CW},25} < (\epsilon_{\text{frac}})_{\text{CW},300} < (\epsilon_{\text{frac}})_{\text{RX},300}$$



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Summary of Results

- Fracture of sheet / cladding controlled by failure of substrate below blister:
 - At 25°C: crack growth on plane normal to σ_1 .
 - At 300°C: shear instability on plane 45° to σ_1 .
- Can we **predict** these results?
 - 25°C----fracture mechanics analysis
 - 300°C---analysis is still incomplete



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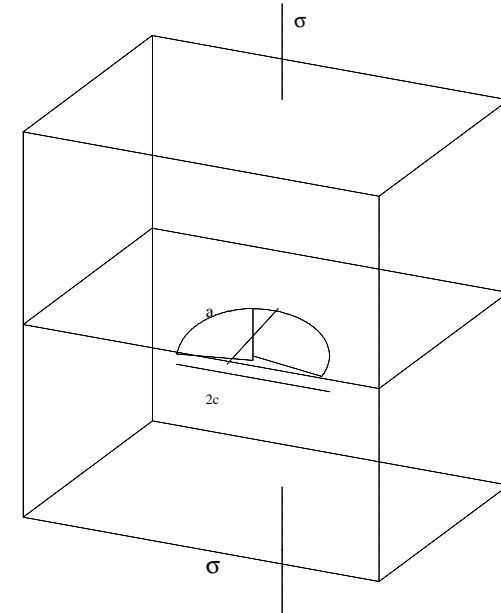
Fracture Mechanics Analysis

■ Assumptions:

- Single crack w/ depth = blister depth
- Through-thickness plane stress conditions
- J-integral procedure
- Plastic zone correction

■ Fracture occurs when:

$$\epsilon_n^p = \alpha \frac{\sigma_0}{E} \left\{ \frac{1}{\alpha} \left(\frac{K_c^2}{K_e^2} - 1 \right) \right\}^{\frac{n}{n-1}}$$

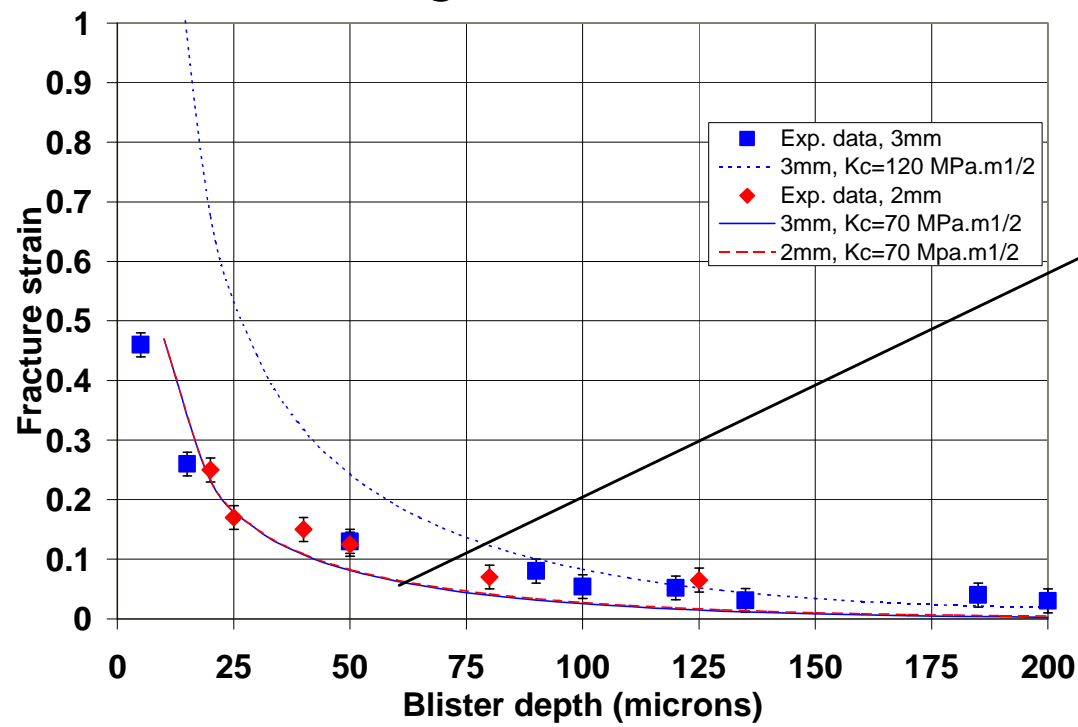




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Fracture Mechanics Analysis

- CWSR material at 25°C with two levels of fracture toughness:



Modeling
similar
for 2mm
and 3mm
wide
cracks



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Fracture Mechanics Analysis

- At 25°C, fracture mechanics predicts exp. results for a reasonable $K_{Ic} \approx 70 \text{ MPa}\cdot\text{m}^{1/2}$, in accordance with fracture profile (crack propagation).
- At 300°C, fracture toughness \uparrow and failure occurs by **competing mechanism**
 \Rightarrow **shear instability** (fracture mechanics no longer applies)



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Summary

Zircaloy w/ 2 or 3 mm-diameter blisters (5 to 250 μ m thick) + hydride precipitates in substrate

- Blisters crack upon yielding.
- As blister depth \uparrow φραχτυρε στραιν \downarrow (ρουγηλψ independent of blister width, $(K_I)_{2mm} \approx (K_I)_{3mm}$)
- For given blister depth:

$$(\epsilon_{frac})_{RX,25} \approx (\epsilon_{frac})_{CW,25} < (\epsilon_{frac})_{CW,300} < (\epsilon_{frac})_{RX,300}$$



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Summary

- Fracture of sheet / cladding controlled by failure of substrate below blister:
 - At 25°C: crack growth on plane normal to σ_1 (predicted for $K_c \approx 70 \text{ MPa}\cdot\mu^{1/2}$).
 - At 300°C: shear instability on plane 45° to σ_1 .
- Fracture of substrate depends on ease of void nucleation at hydrides. At 25°C, hydrides crack / voids coalesce. Not so at 300°C where $(\epsilon_N)_{300} > (\epsilon_N)_{25}$ and shear instability develops.